

2014 VR&D Design Optimization Users' Conference
Portola Plaza, Monterey, CA



GENESIS Structural Optimization Software: Current and Upcoming New Features

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Vanderplaats Research & Development, Inc.

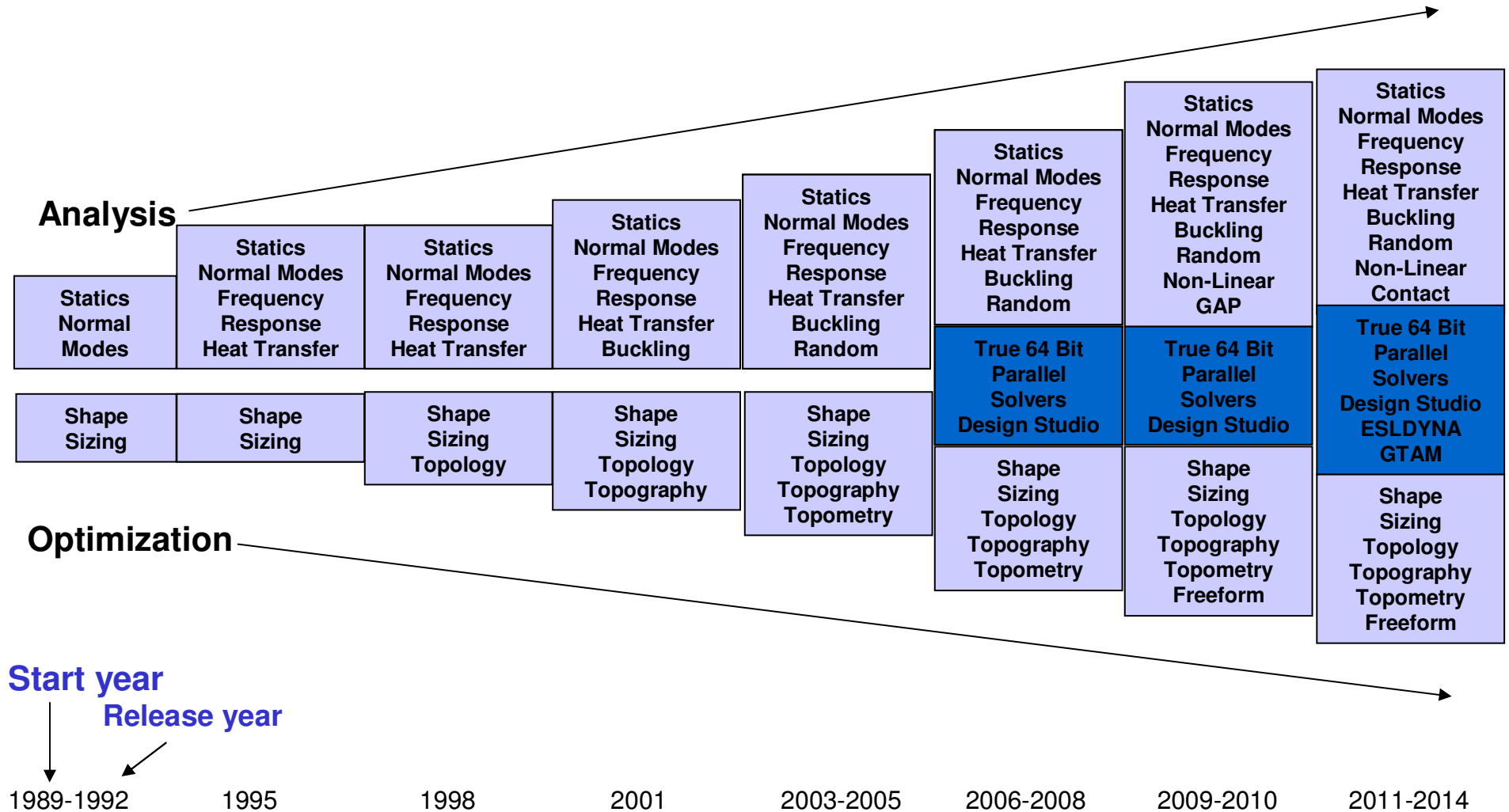
October 27, 2014

Outline



- **GENESIS Evolution**
- **Enhancements in GENESIS 13 and 13.1**
 - Finite Element Enhancements
 - Optimization Enhancements
- **Upcoming Features in GENESIS 14**
 - Finite Element Enhancements
 - Optimization Enhancements
- **Concluding Remarks**

GENESIS Evolution





Finite Element Enhancements in 13.0 and 13.1

Finite Elements Improvements



- **Non-Linear Contact Analysis**

- Automatically generates potential contact points from surface definitions
- Works with static load cases
- Different static load case can have different contact conditions in the same run
- Much easier than using CGAP elements
- Accurate contact pressure results

Contact Analysis

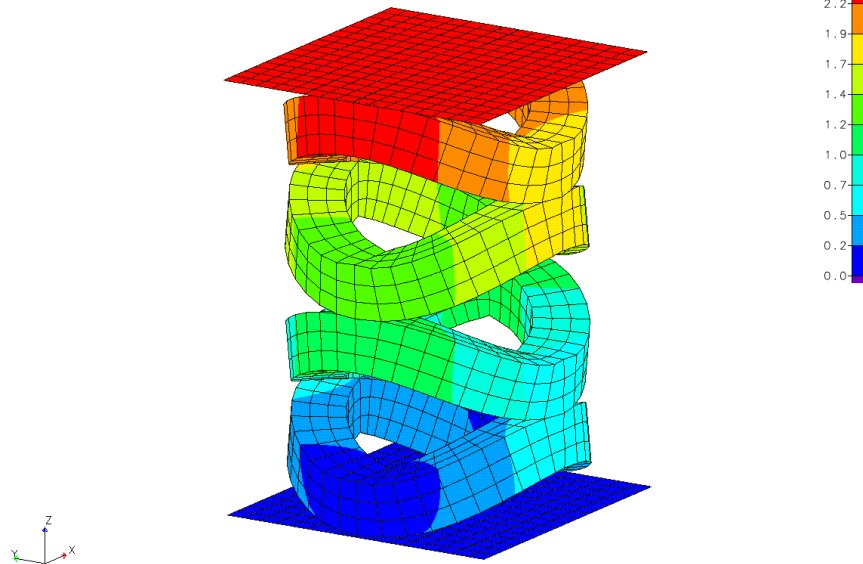


- **Surface to surface contact**
 - Solid surface to solid surface
 - Solid surface to shell surface
 - Shell surface to shell surface
- **Contact surface definition by**
 - Material ID's (BSURFM)
 - Element properties (BSURFP)
 - Element ID's (BSURFE)
- **Post-processing output**
 - Contact pressure
 - Contact force
 - Contact clearance

Contact Analysis Examples

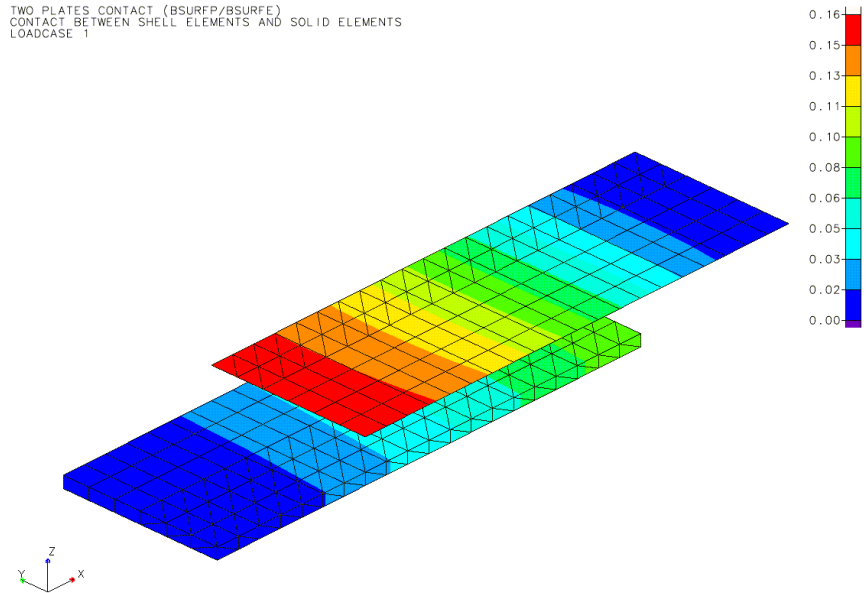


RING SPRING CONTACT
LOADCASE 1



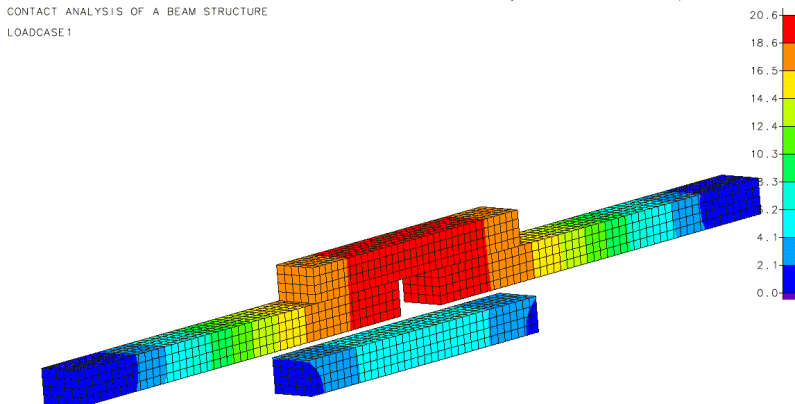
Cycle 0 Loadcase 1 Displacement XYZ Magnitude

TWO PLATES CONTACT (BSURFP/BSURFE)
CONTACT BETWEEN SHELL ELEMENTS AND
LOADCASE 1



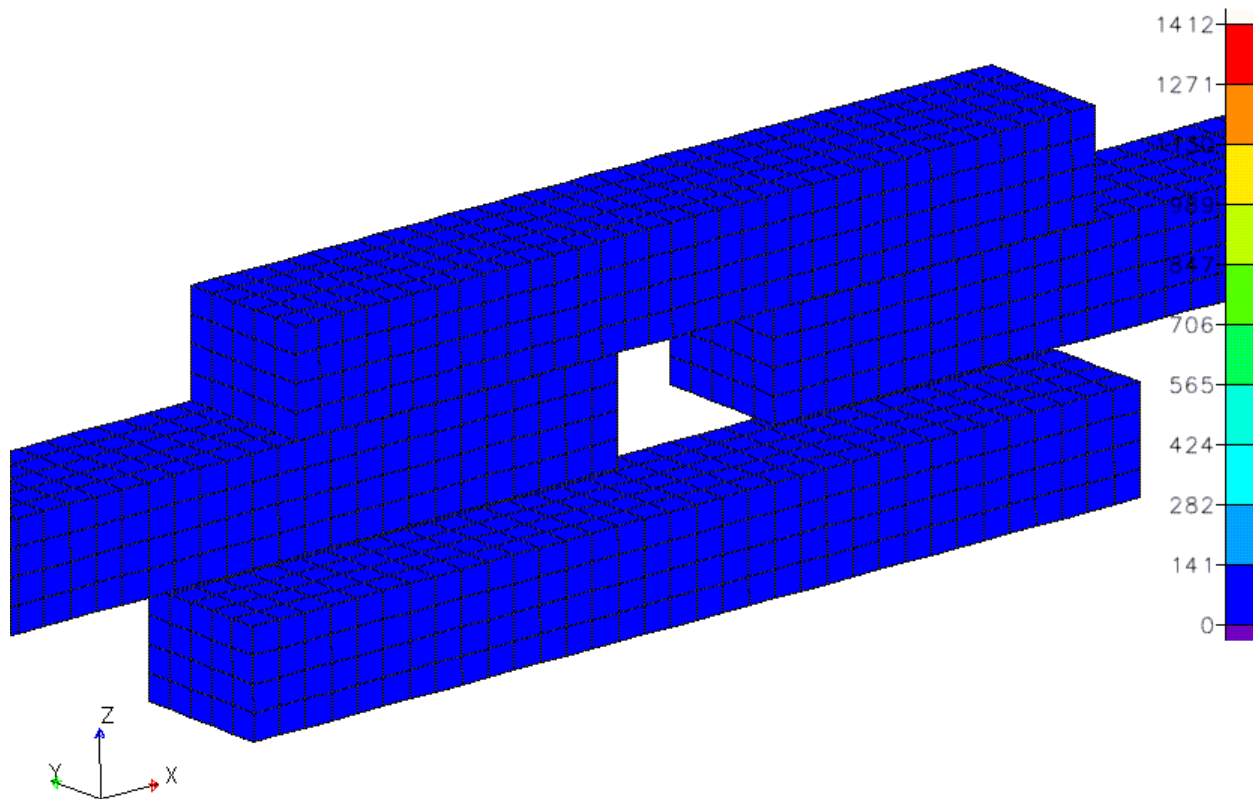
Cycle 0 Loadcase 1 Displacement XYZ Magnitude

CONTACT ANALYSIS OF A BEAM STRUCTURE
LOADCASE 1



Cycle 0 Loadcase 1 Displacement XYZ Magnitude

Contact Analysis Examples



Equivalent Radiated Power



- **ERP Assumption:**

The pressure at the structure-fluid interface is proportional to the normal velocity times the fluid density times the speed of sound in the fluid.

$$ERP = \frac{1}{2} \rho c \iint_A v_n^* v_n dA$$

where:

ρ is the fluid density

c is the speed of sound in the fluid

v_n is the component of the velocity normal to the structural panel

v_n^* is the complex conjugate velocity

A is the panel area

- Note that ERP is an implicit function of the loading frequency, ω



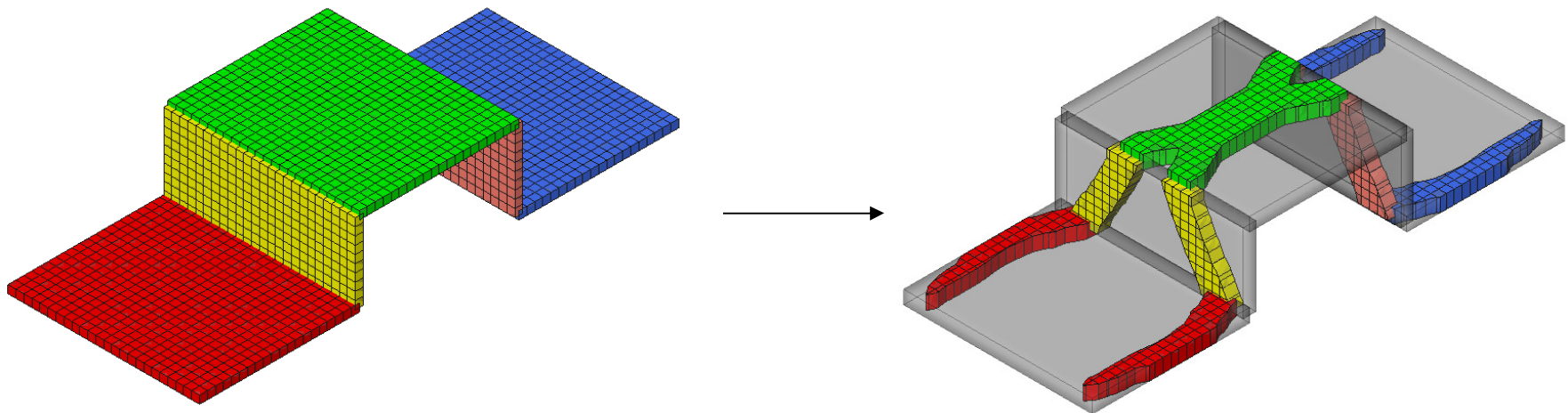
Optimization Enhancements in 13.0 and 13.1

Optimization Enhancements



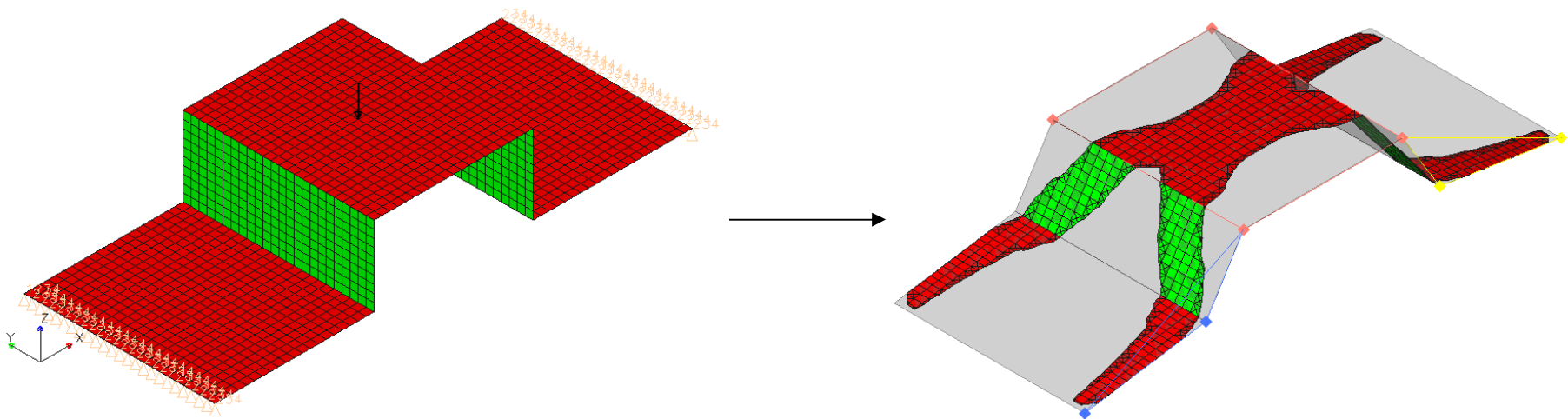
- **Topology Optimization is now Integrated with Parametric Optimization**
 - Topology can be mixed with Sizing, Shape, Topometry, Topography and/or Freeform
 - DRESP1 and other Parametric entries can be used simultaneously with TRESP1 and other Topology entries

Mixed Topology and Sizing



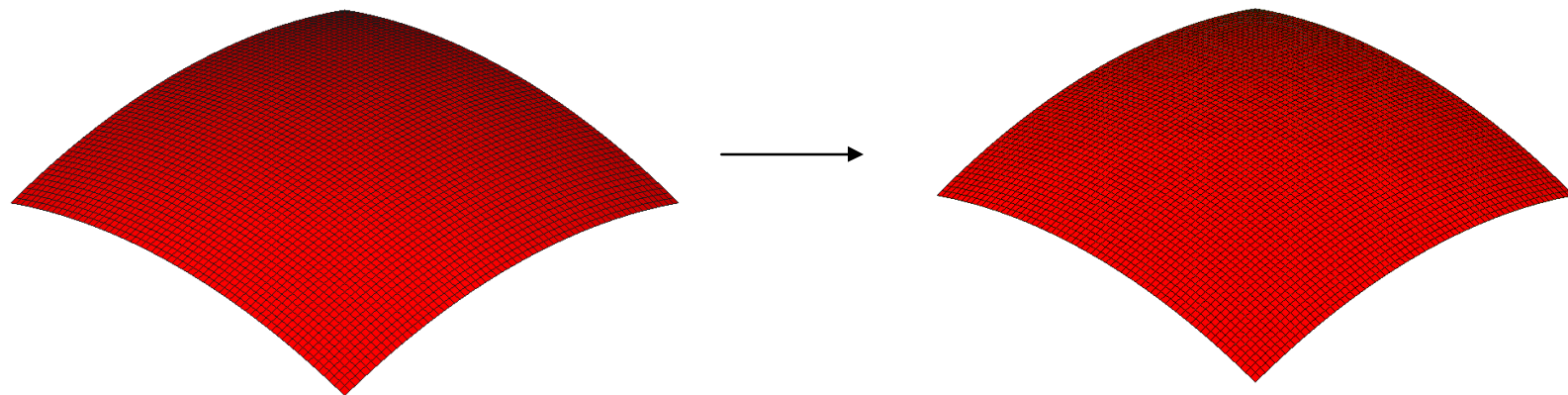
Topology & Sizing Optimization

Mixed Topology and Shape



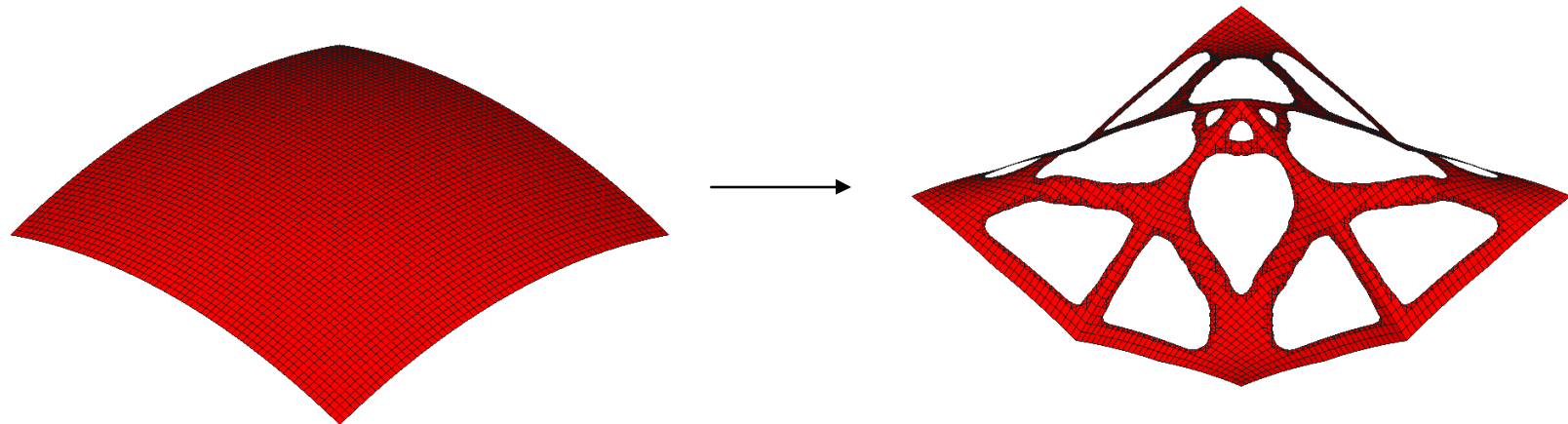
Topology & Shape Optimization

Mixed Topology and Shape



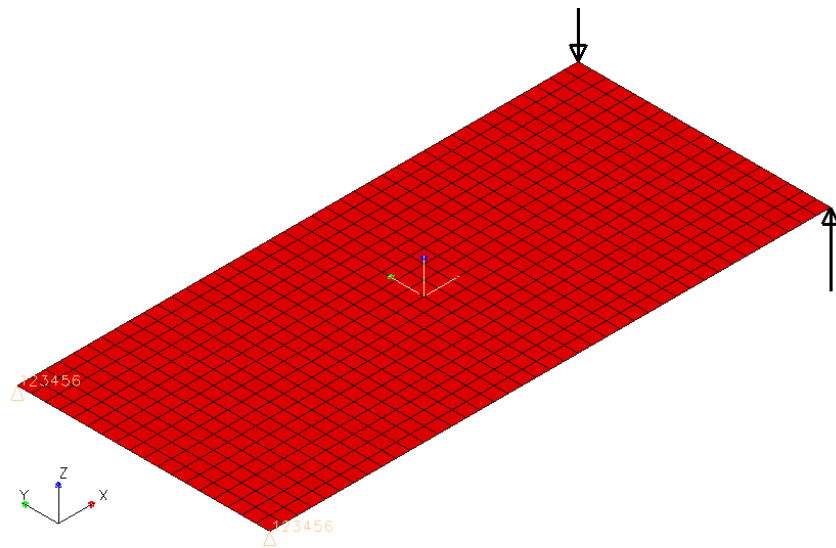
Topology & Shape Optimization

Mixed Topology and Shape

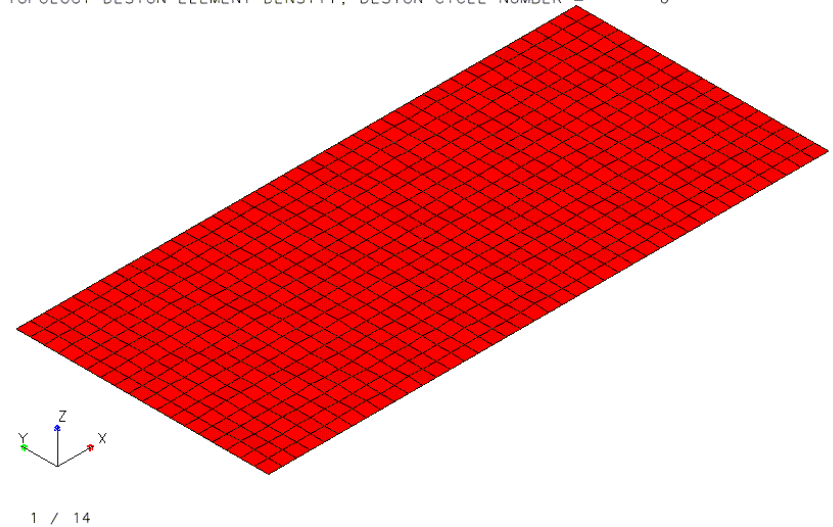


Topology & Shape Optimization

Mixed Topology and Freeform



BEAD PATTERN OPTIMIZATION USING FREEFORM AND GRIDFR
STRAIN ENERGY MINIMIZATION TO INCREASE OVERALL STIFFNESS
TOPOLOGY DESIGN ELEMENT DENSITY, DESIGN CYCLE NUMBER = 0



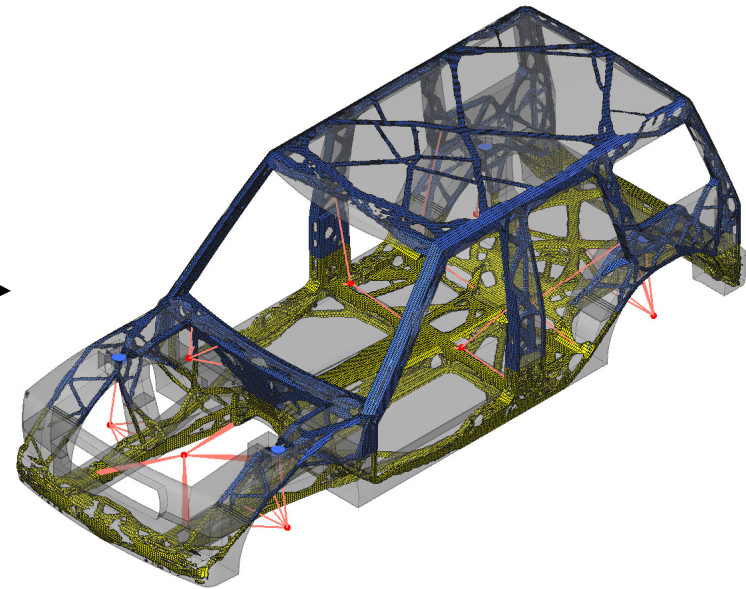
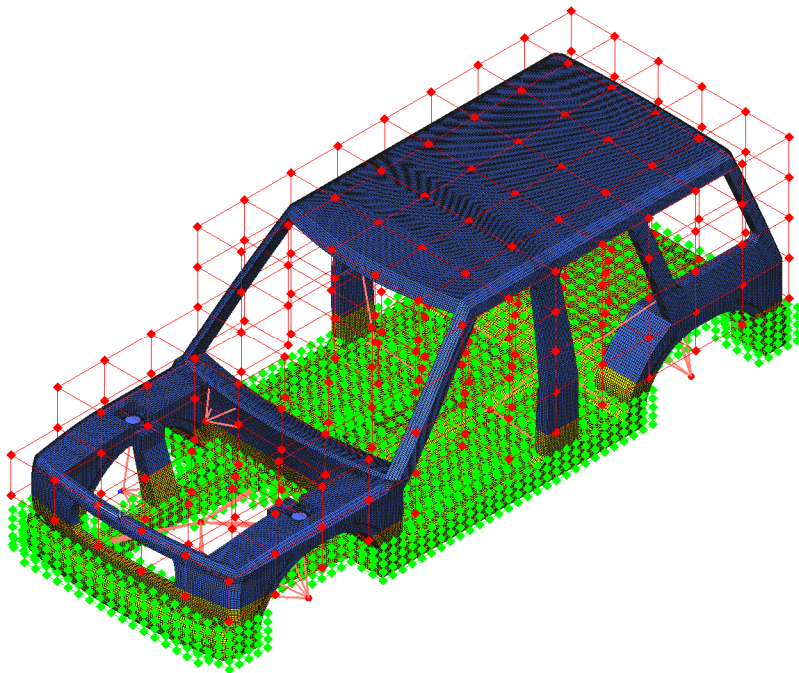
Topology & Freeform Optimization

Mixed Topology and Freeform



- Minimize SE with mass fraction of 0.1
- 10 static loadcases
- 737,836 Topology design variables
- 1,477 shape design variables
- Mass constraint $\leq \text{Initial mass} \cdot 0.01$

BODY IN WHITE SOLID ELEMENT TOPOLOGY BLANK MODEL
MF=0.10, INERTIA RELIEF IMPACT CASES
TOPOLOGY DESIGN ELEMENT DENSITY, DESIGN CYCLE NUMBER = 26
Isosurface enclosing 13% of topology region



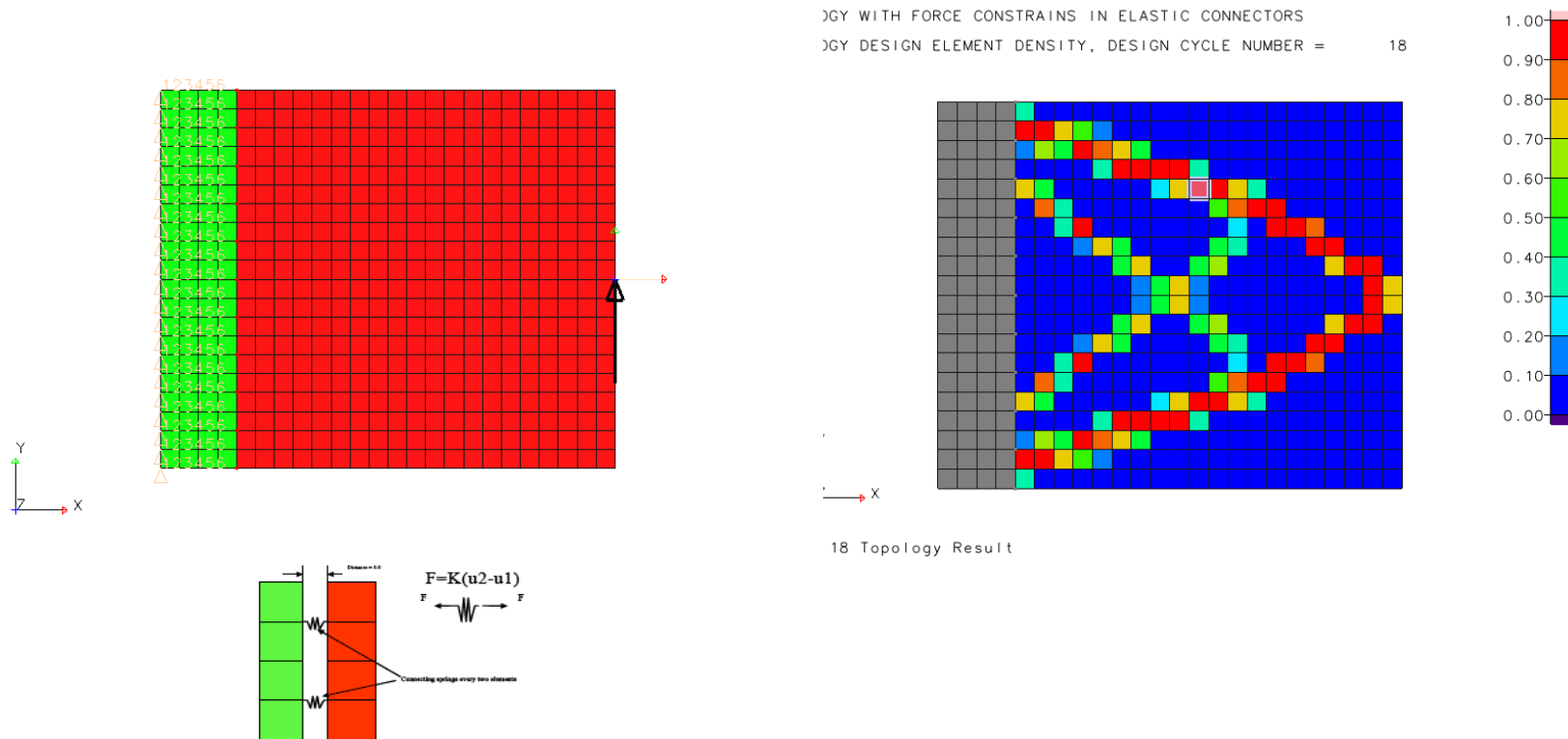
Cycle 26 Topology Result

Topology & Freeform Optimization

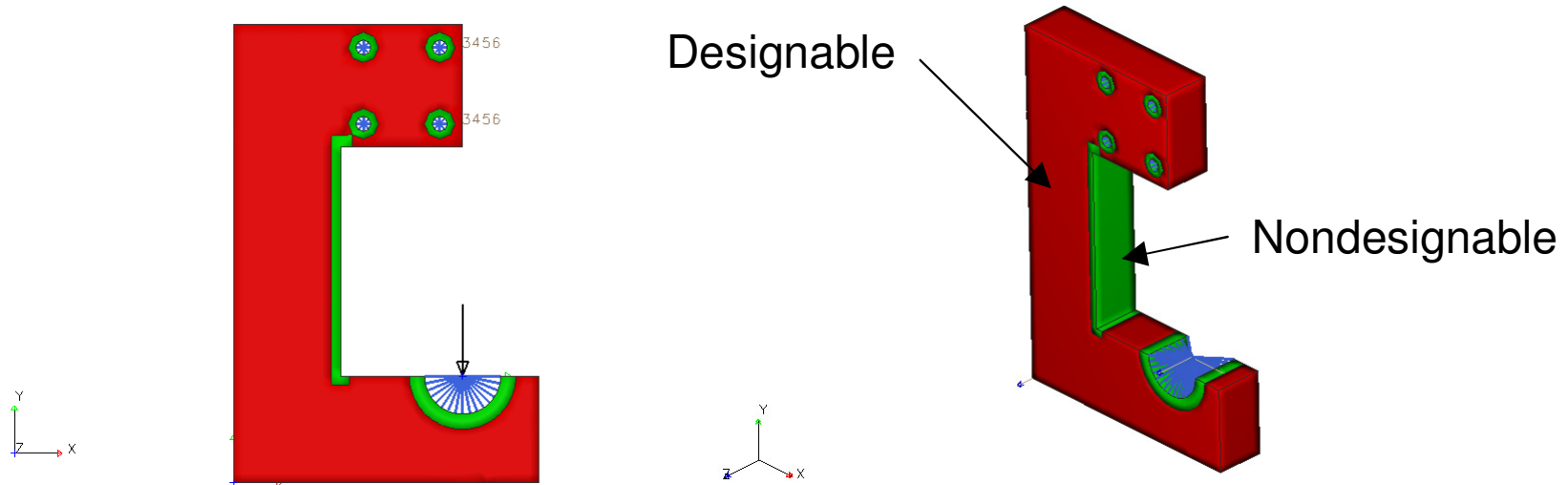
Topology with DRESP1



Topology with Forces Constraints in CELAS Connectors



Topology with Stress Constraints



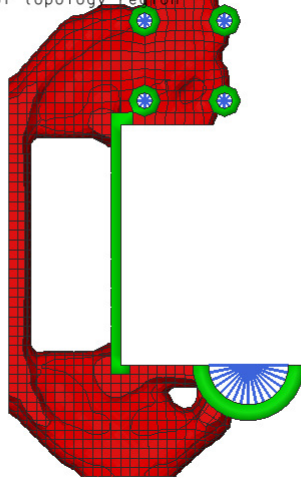
Topology with Stress Constraints



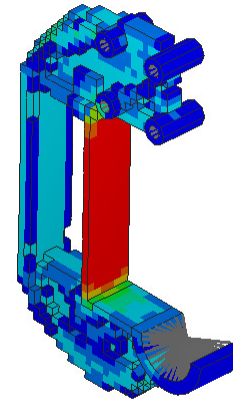
SOLID TOPOLOGY TUTORIAL
TOPOLOGY DESIGN ELEMENT DENSITY, DESIGN CYCLE NUMBER =
Isosurface enclosing 39% of topology result

16

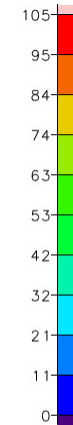
SOLID TOPOLOGY TUTORIAL
LOADCASE 1



Cycle 16 Topology Result



Cycle 16 Loadcase 1 Solid Stress Von Mises



Reference Answer
Without stress constraints
Max Stress = 105 MPa



Finite Element Enhancements in 14.0

Finite Element Improvements



- **Glue-Like Connections**

- Automatically generates glue connection from surface definitions
- Works with Natural frequency loadcases and Frequency responses
- Different loadcases can have different glue-like conditions in the same run

Finite Element Improvements



- **Non-Linear Contact Improvements**
 - Internal algorithm that calculates contact areas has been refined. This help to produce better answers on problems with bad meshes
 - Convergence history now is output so that users can see the progress in solving the non-linear problem

Finite Element Improvements



- **Status and Progress on Contact and Glue Connections**

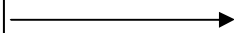
	V12.0	V12.2	V13.0	V14.0
Non-Linear Gap	yes	yes	yes	yes
Glue Connections	no	yes	yes	yes
Non-Linear Contact	no	no	yes	yes
Axisymmetric Glue-Connections	no	no	yes	yes
Glue-Like Connections	no	no	no	yes

Finite Element Improvements



- **New 5-Node and 13-Node Pyramidal Elements**

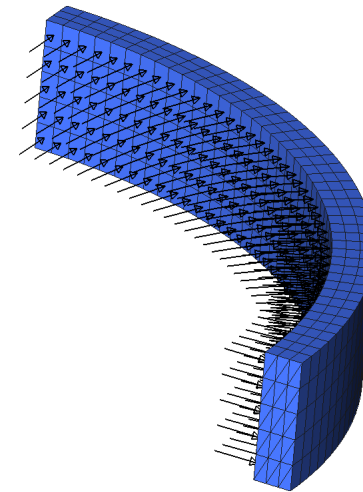
CPYRA



PSOLID

Analysis Updates

- Element stiffness matrices
- Lumped and Consistent mass matrices
- Conductivity matrices
- Geometric stiffness
- Damping matrices

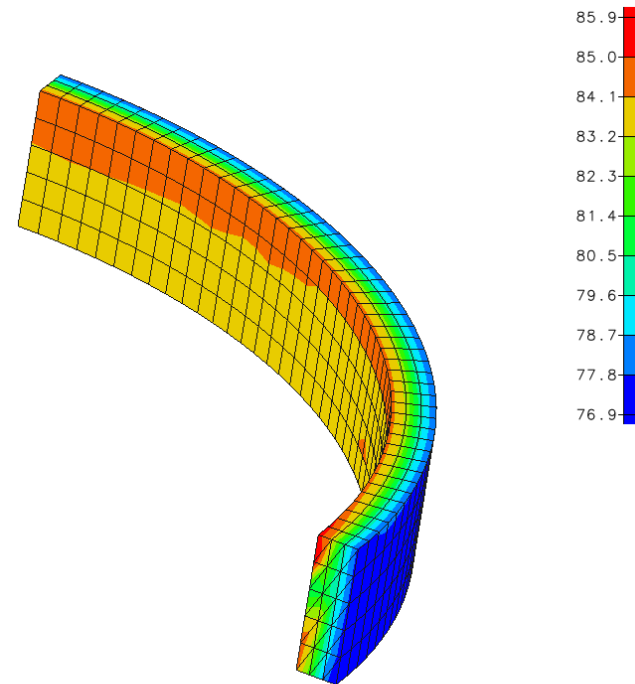


New Finite Element Results



- Statics, Freq. Resp. and Random Stress/Strain Recovery for the new **5-node and 13-Node CPYRA element**
- Static and Freq. Resp. GSTRESS for the new **5-node and 13-Node CPYRA element**

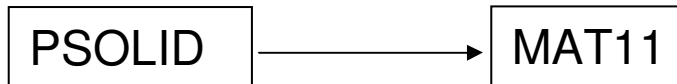
STRESS=ALL
STRAIN=ALL
GSTRESS=ALL



Finite Element Improvements



- **New orthotropic Material: MAT11**



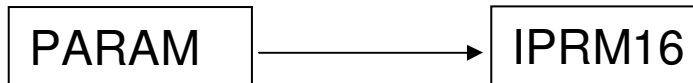
Analysis Updates

- Any solid element can now use orthotropic material

Finite Element Improvements



- **Output Element Stiffness Matrix and Mass Matrix to DMIG format**



IPRM16=10 → output K matrices

IPRM16=20 → output M matrices

IPRM16=30 → output K and M matrices

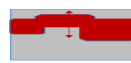


Optimization Enhancements in 14.0



Families of Manufacturing Constraints

Castings



FGZ



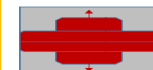
FBZ



FTZ



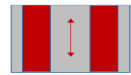
FSZ



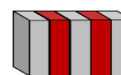
F0Z

New

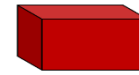
Extrusion and
Uniforms



EZ

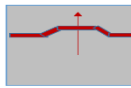


UZX

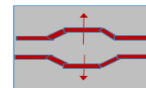


UXYZ

Stamping

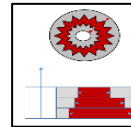


S1Z

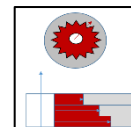


S2Z

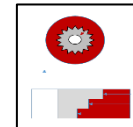
Radial Filling



RGZ



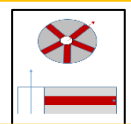
RBZ



RTZ

New

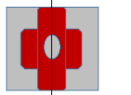
Radial Spokes



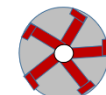
KZ

New

Mirror & Cyclic Symmetry

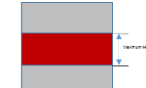
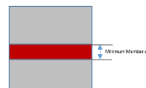


MZX



CX

Minimum & Maximum Member Size

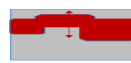


New



Family of Manufacturing Constraints

Castings



FGZ



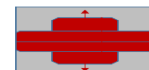
FBZ



FTZ



FSZ

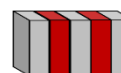


F0Z

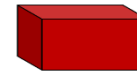
Extrusion and
Uniforms



EZ

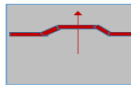


UZX

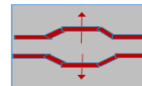


UXYZ

Stamping

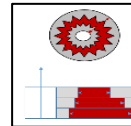


S1Z

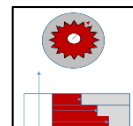


S2Z

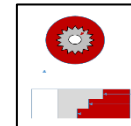
Radial Filling



RGZ

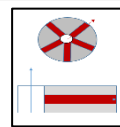


RBZ



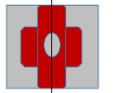
RTZ

Radial Spokes

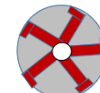


KZ

Mirror and Cyclic Symmetry

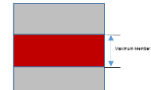
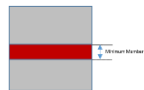


MZX



CX

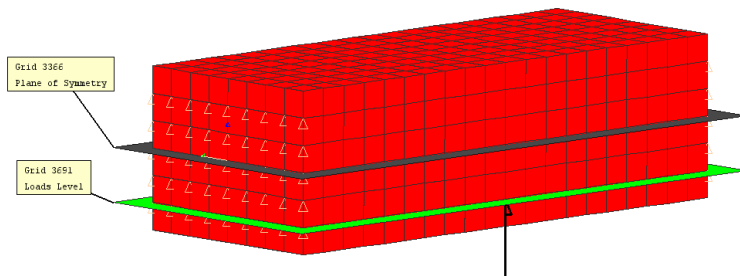
Minimum & Maximum Member Size



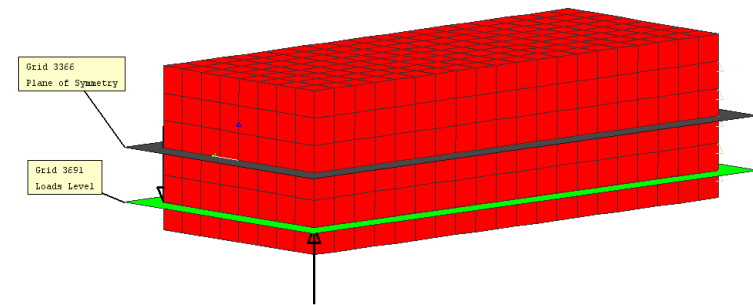
Design of Structure Subject to 3 Torsion Loadcases



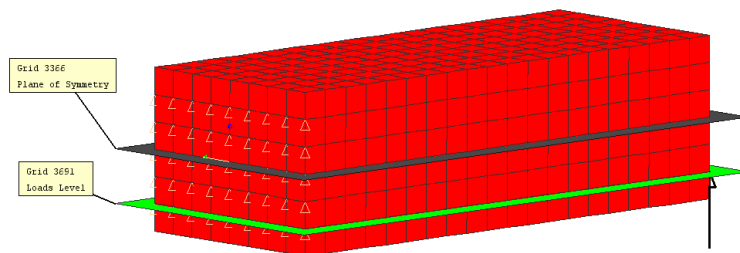
Example: new F0Z



Loadcase 1: Torsion Center



Loadcase 2: Torsion End A

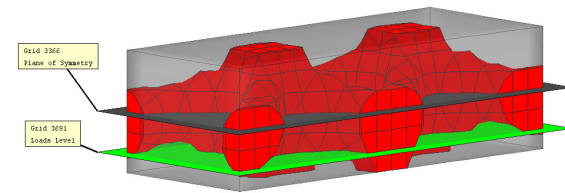
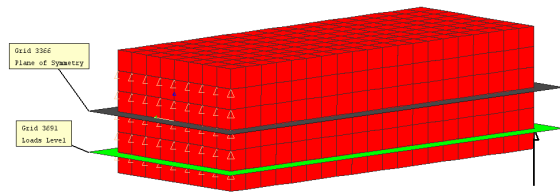


Loadcase 3: Torsion End B

Design of Structure Subject to 3 Torsion Loadcases

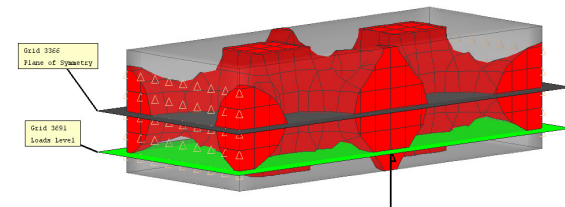


Example: new F0Z



Optimum using Existing FGZ

Answer is not Symmetric
w/r to Parting Plane





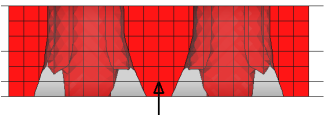
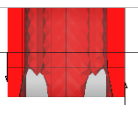
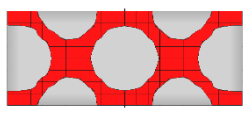
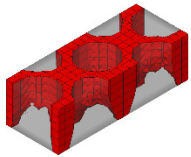


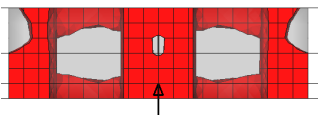

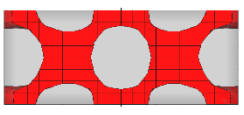
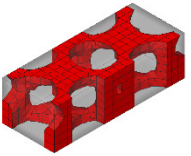


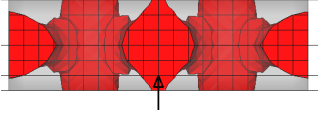
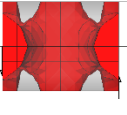
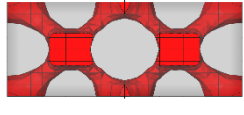
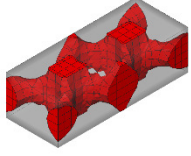


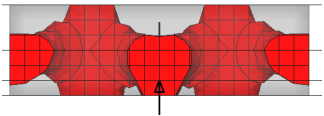
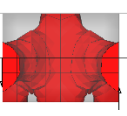
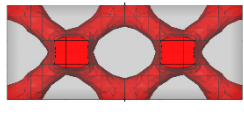
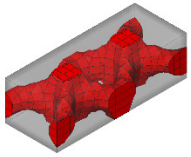


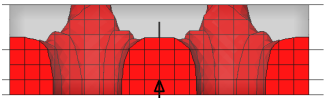

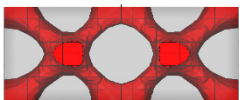
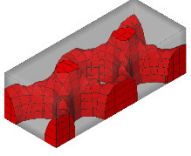
Optimum using New F0Z

Answer is Symmetric
w/r to Parting Plane

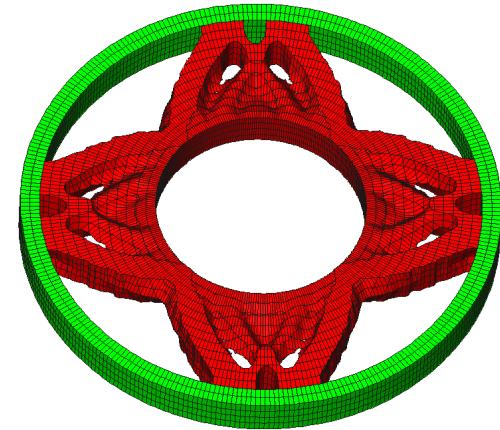
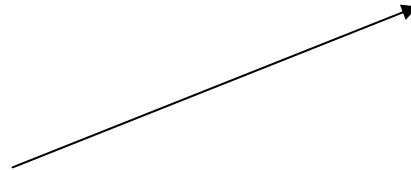
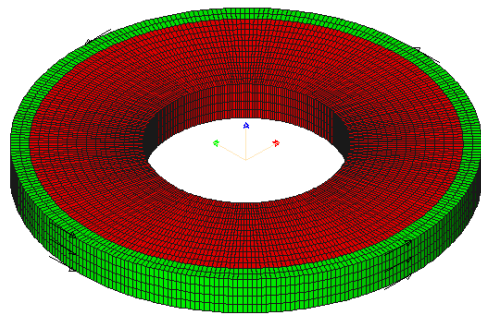
Design of Structure Subject to 3 Torsion Loadcases



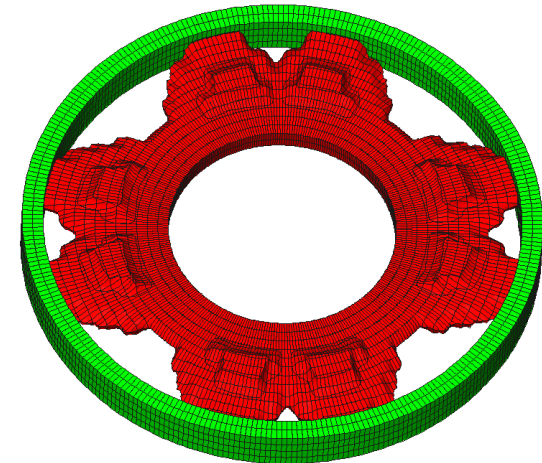
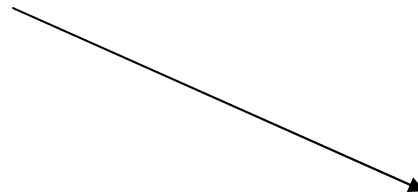
Four Views of Five Alternative Designs using Different Filling Fabrication Constraints

Type	Filling Direction	Side View	Front View	Top View	ISO View
FTZ 					
FSZ 					
F0Z 					
FGZ 					
FBZ 					

New Manufacturing Constraints: RGZ

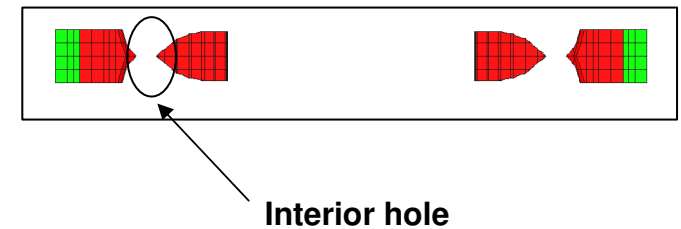
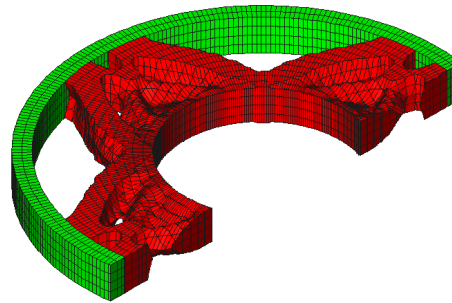
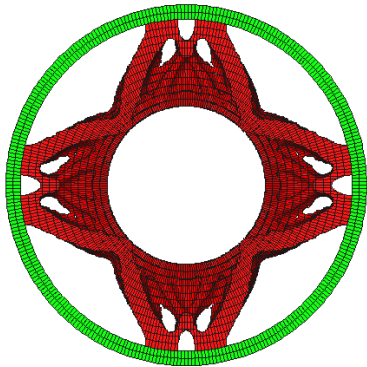


Free Topology: Reference Answer

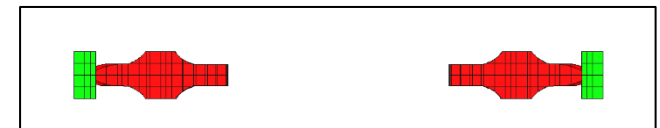
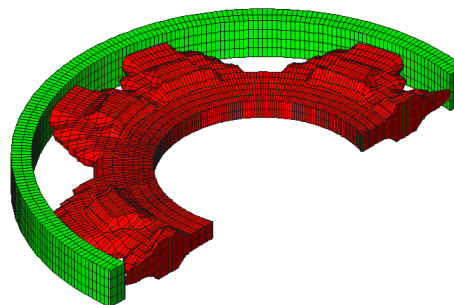
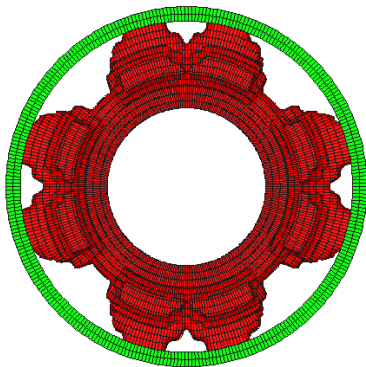


Topology with Radial Filling: RGZ

New Manufacturing Constraints: RGZ



Free Topology: Reference Answer

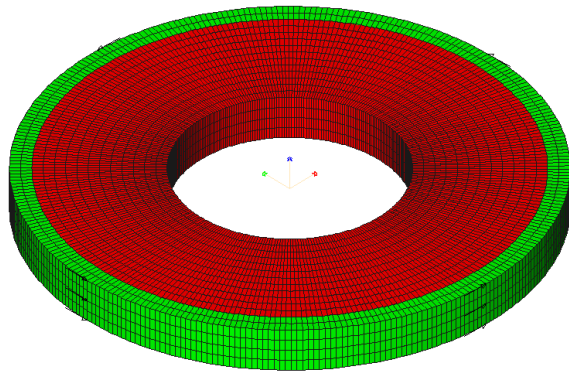


Topology with Radial Filling: RGZ

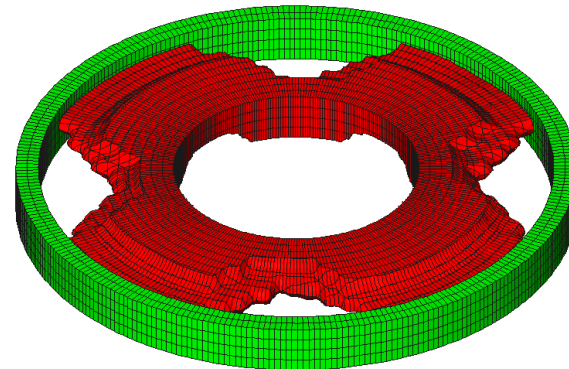
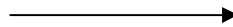
New Manufacturing Constraints: RBZ



Topology with Radial Filling from Bottom: RBZ



Initial Design

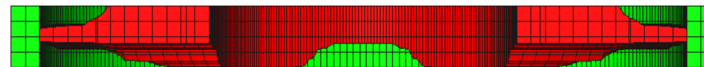
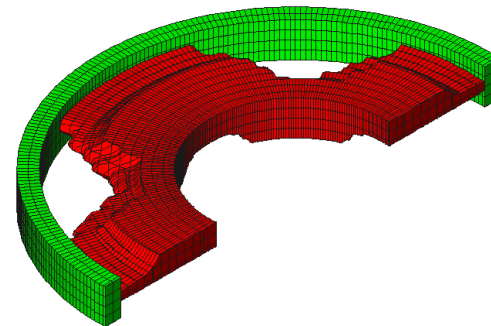
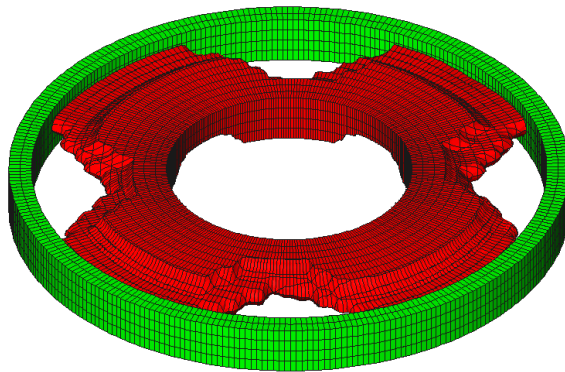


Topology with Radial Filling from Bottom: RBZ

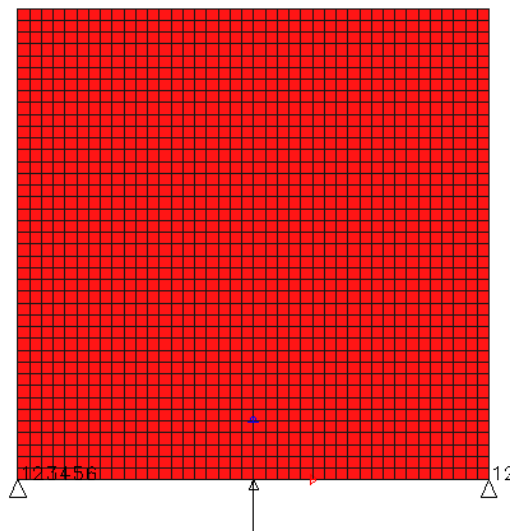
New Manufacturing Constraints: RBZ



Topology with Radial Filling from Bottom: RBZ

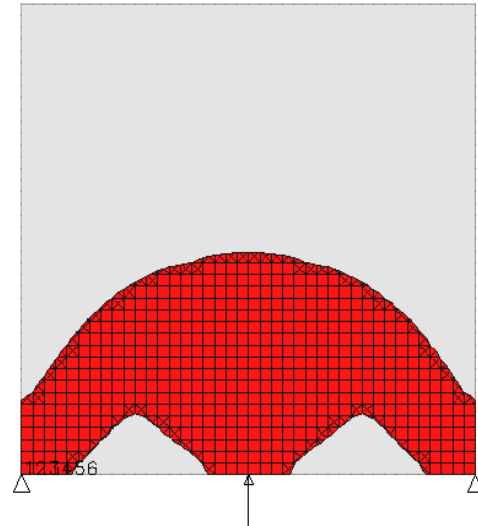


Shell Structure with Maximum Member Size



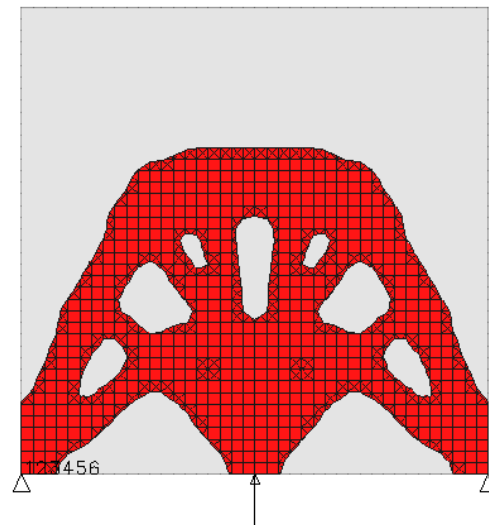
Initial Design

Topology Optimization



W/O Maximum Member Size Control

Topology Optimization

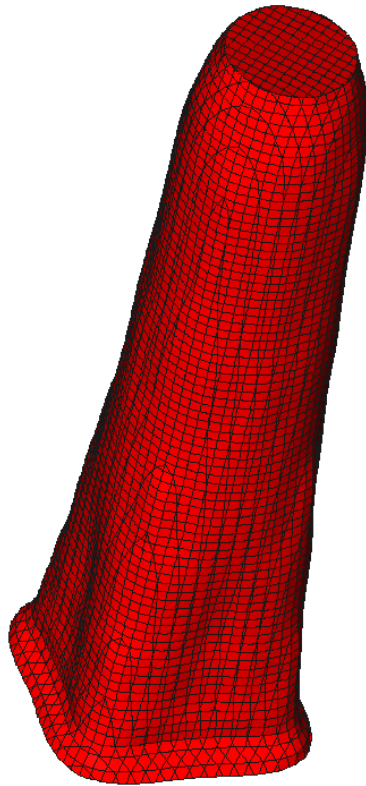


With Maximum Member Size Control

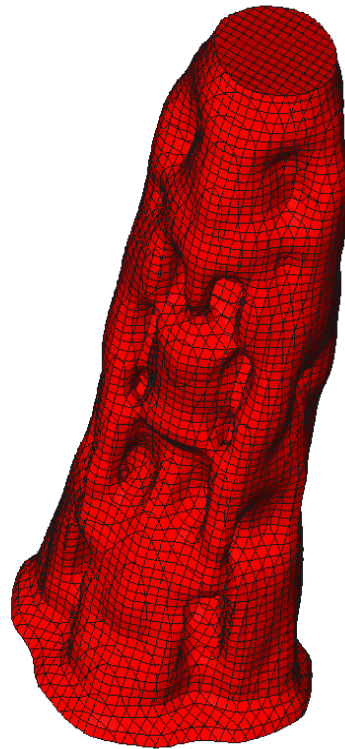
Solid Structure with Maximum Member Size



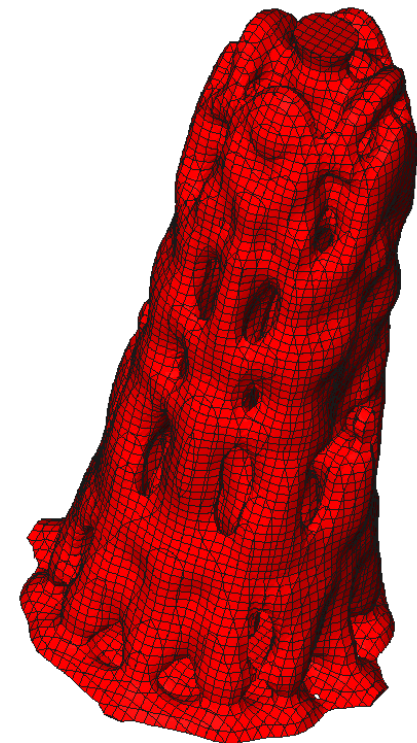
Three Alternative Topology Designs



Free Topology
W/O Max. Size Control



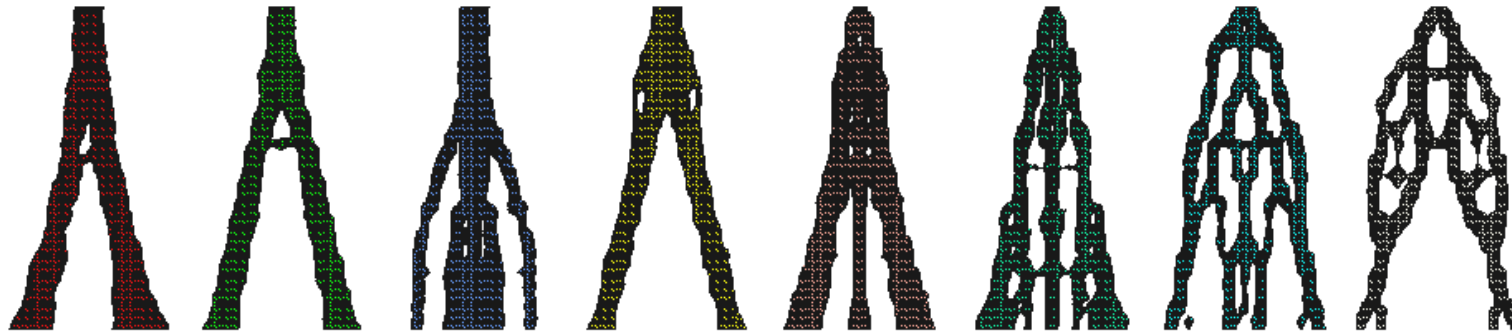
Max Member Size=1.0
Minimum GAP=1.0



Max Member Size=0.5
Minimum GAP=0.5

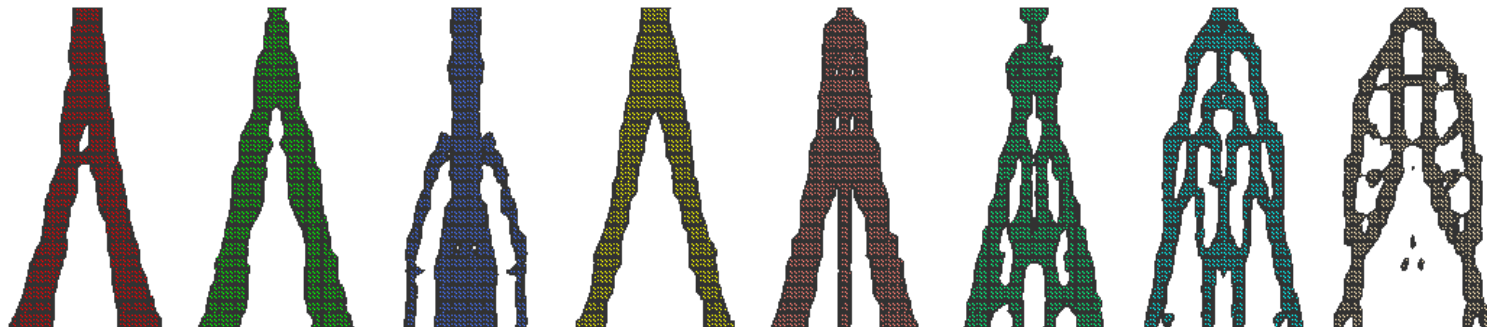


Alternative Designs Using Different Values for Maximum Member Size and Minimum Gap



TRIA3

MMS=1.0 MG = 1.0	MMS=1.0 MG = 2.0	MMS=1.0 MG = 3.0	MMS=1.0 MG = 4.0	MMS=0.5 MG = 0.5	MMS=0.5 MG = 1.0	MMS=0.5 MG = 1.5	MMS=0.5 MG = 2.0
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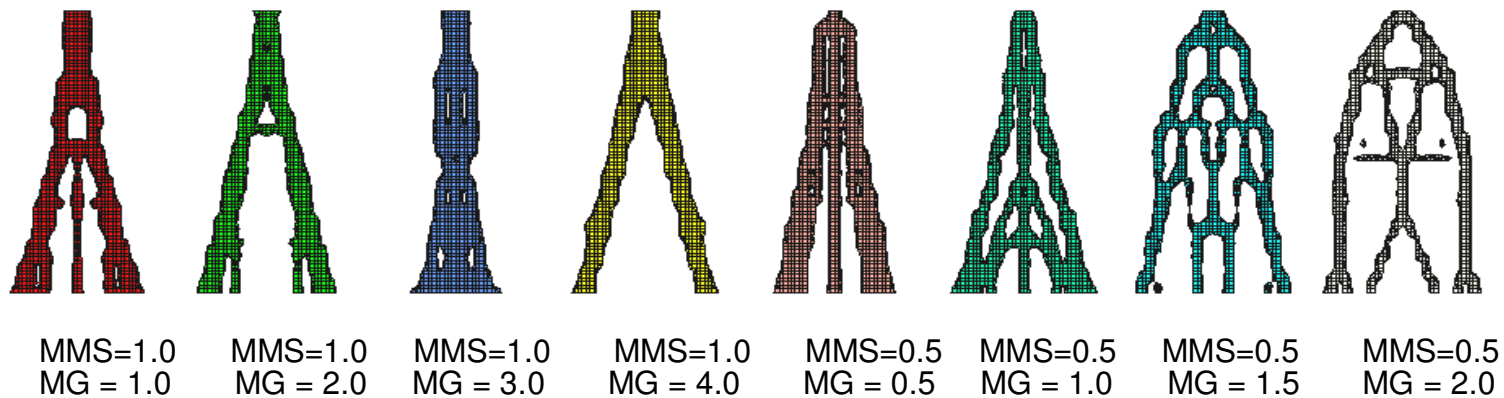
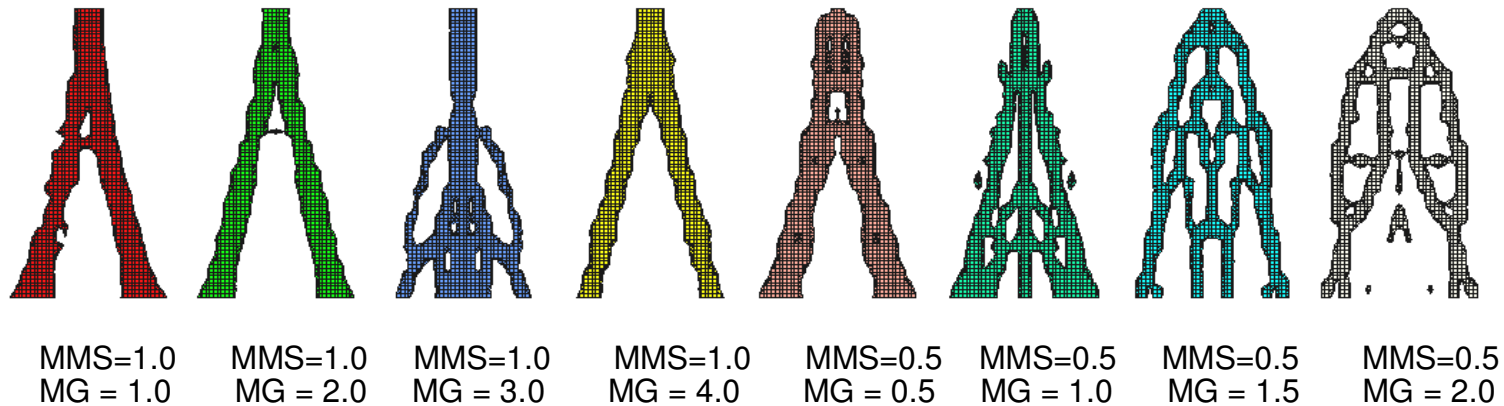


TRIA6

MMS=1.0 MG = 1.0	MMS=1.0 MG = 2.0	MMS=1.0 MG = 3.0	MMS=1.0 MG = 4.0	MMS=0.5 MG = 0.5	MMS=0.5 MG = 1.0	MMS=0.5 MG = 1.5	MMS=0.5 MG = 2.0
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------

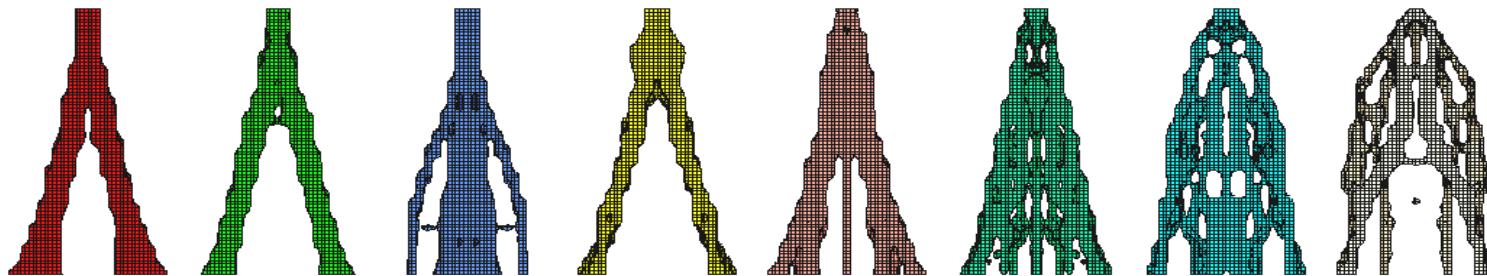


Alternative Designs Using Different Values for Maximum Member Size and Minimum Gap



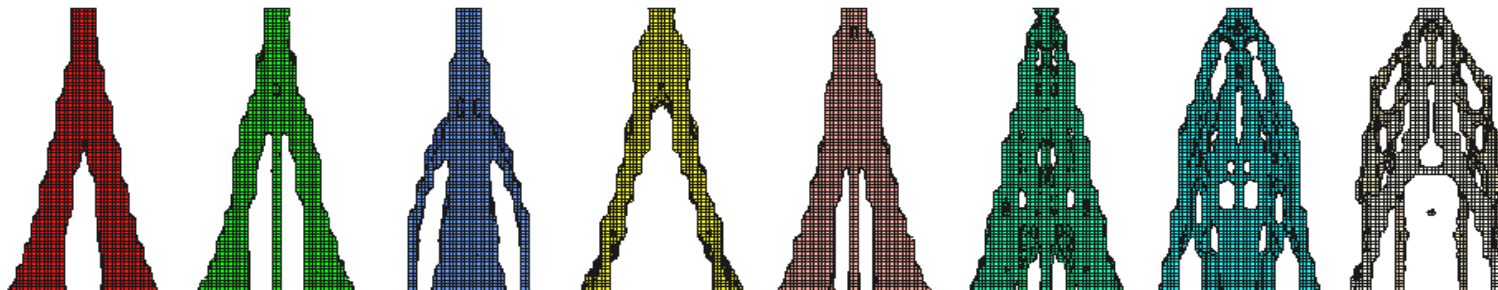


Alternative Designs Using Different Values for Maximum Member Size and Minimum Gap



HEXA

MMS=1.0 MG = 1.0	MMS=1.0 MG = 2.0	MMS=1.0 MG = 3.0	MMS=1.0 MG = 4.0	MMS=0.5 MG = 0.5	MMS=0.5 MG = 1.0	MMS=0.5 MG = 1.5	MMS=0.5 MG = 2.0
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HEX20

MMS=1.0 MG = 1.0	MMS=1.0 MG = 2.0	MMS=1.0 MG = 3.0	MMS=1.0 MG = 4.0	MMS=0.5 MG = 0.5	MMS=0.5 MG = 1.0	MMS=0.5 MG = 1.5	MMS=0.5 MG = 2.0
---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------	---------------------

Additional Enhancements in 14.0



- **Topology Optimization now supports solid anisotropic (MAT9) and orthotropic (MAT11) materials**
- **Topology Optimization now supports composite (PCOMP) elements**
- **The approximate problem now is much faster for problems with linear constraints**

Conclusions



- ***GENESIS* is Continuously Being Improved for Functionality**
- **Numerous User-Requested Features have been Added**

Conclusions



- **Design Studio Has Been Upgraded to Support *GENESIS* 14.0**

Questions?



Thanks for Attending